

TITLE OF THE INVENTION

METHOD OF ADJUSTING PROJECTION OPTICAL APPARATUS

BACKGROUND OF THE INVENTION

Field of the Invention

5 The present invention relates to a projection optical apparatus for projecting and exposing the pattern of a first object on a second object and, more particularly, to a method of adjusting the projection optical apparatus.

10 Related Background Art

 A projection optical system used in an exposure apparatus that prints a precision circuit pattern on a substrate (wafer, plate, or the like) coated with a photosensitive material requires very high optical performance. For this purpose, optical members used in the projection optical system are manufactured with an ultimately high manufacturing precision.

 When manufactured optical members are combined to assemble a projection optical system, very fine adjustment is performed such as adjusting the distances between the respective optical members by changing the thicknesses of washers between lens barrels holding the respective optical members, tilting the optical members (rotating the optical members about, as an axis, a direction perpendicular to the optical axis), or shifting the optical members (moving the optical

members in a direction perpendicular to the optical axis), while actually measuring the aberration of the projection optical system. This adjustment minimizes degradation in optical performance which is caused by the manufacturing error of the optical members or which occurs during assembly of the optical members.

SUMMARY OF THE INVENTION

According to the present invention, there is provided an adjusting method having the first step of measuring the residual distortion component of a projection optical system having a predetermined target member in its optical path, the second step of calculating, based on the measurement result of the first step, the surface shape of the target member which cancels the residual distortion component, the third step of removing the target member from the projection optical system and machining the target member so as to have the surface shape calculated in the second step, and the fourth step of inserting the target member machined in the third step into the optical path of the projection optical system.

The present invention will be more fully understood from the detailed description given hereinbelow and the accompanying drawings, which are given by way of illustration only and are not to be considered as limiting the present invention.

Further scope of applicability of the present invention will become apparent from the detailed description given hereinafter. However, it should be understood that the detailed description and specific examples, while indicating preferred embodiments of the invention, are given by way of illustration only, since various changes and modifications within the spirit and scope of the invention will be apparent to those skilled in the art from this detailed description.

BRIEF DESCRIPTION OF THE DRAWINGS

Figs. 1 and 2 are views for explaining the principle of an adjusting method according to the present invention, in which Fig. 1 shows the state of a beam before adjustment, and Fig. 2 shows the state of a beam after adjustment;

Fig. 3 shows the schematic arrangement of an exposure apparatus to which the adjusting method of the present invention is applied;

Fig. 4 shows the arrangement of a holding member that holds a distortion correction plate;

Fig. 5 is a plan view showing the arrangement of a test reticle used for measuring various aberrations other than distortion;

Fig. 6 is a plan view showing the arrangement of a test reticle used for measuring distortion;

Fig. 7 shows the state of a pattern on a wafer

which is formed by using the test reticle shown in Fig. 6;

Figs. 8 and 9 are graphs for explaining a curved surface interpolation equation of this embodiment, in which Fig. 8 shows a case wherein a conventional curved surface interpolation equation is used, and Fig. 9 shows a case wherein a curved surface interpolation equation of this embodiment is used;

Figs. 10 to 14 show a curved surface interpolation method of this embodiment;

Fig. 15 shows the arrangement of an apparatus that machines the distortion correction plate;

Fig. 16 briefly shows the adjusting method according to the present invention; and

Fig. 17 briefly shows a method of calculating the shape of the distortion correction plate from distortion data.

DESCRIPTION OF THE PREFERRED EMBODIMENT

In the conventional projection optical system, distortion components are present that cannot be corrected even by assembly adjustment as described above. Of all the distortion components, regarding in particular a random component (asymmetric distortion) not having a directionality with respect to an optical axis serving as the reference, no effective correcting method is conventionally available for such a random

component, and this random component interferes with an improvement in total overlay of a precision printing exposure apparatus.

On the other hand, in the present invention having the above arrangement, as the surface of a target member serving as an optical member partly constituting the projection optical system is machined, a beam that passes through this target member can be deflected by refraction. Thus, an imaging position at a predetermined point on the surface of an object is deflected on an image surface in a direction perpendicular to the optical axis, so that a residual magnification component and a residual distortion component in the projection optical system can be corrected.

Assuming an ideal imaging position of a projection optical system which is an ideal optical system having no aberration, a residual distortion component is a shift amount between the actual imaging position of a beam formed through a target member and a projection optical system, and an ideal imaging position.

The principle of the present invention will be described with reference to the accompanying drawings. Fig. 1 is a view showing a target member 10 before machining arranged between a reticle R and a wafer W. In Fig. 1, the projection optical system is omitted.

Referring to Fig. 1, a beam emerging from a point O on the reticle R forms an image on the wafer W through the target member 10 and the projection optical system (not shown). When the projection optical system (not shown) has distortion, the beam emerging from the point O on the reticle R is focused on a point P_1 to form the image of the point O at the point P_1 . When the projection optical system (not shown) is an ideal imaging optical system, a beam emerging from the point O on the reticle R is focused on a point P_0 to form the image of the point O at the point P_0 . At this time, the shift between the points P_0 and P_1 within the surface of the wafer W corresponds to the distortion of the projection optical system.

In the present invention, as shown in Fig. 2, the surface of the target member 10 present in the optical path of the projection optical system is machined so that it is changed from a surface 10a before machining to a surface 10b. Then, the beam emerging from the point O on the reticle R is refracted by the surface 10b of the target member 10, and is thus focused on the point P_0 on the wafer W. Hence, the distortion of the projection optical system is corrected.

In the present invention, it is desirable that the various aberrations that occur symmetrically with respect to the optical axis are corrected before

correction by means of the target member is performed. Then, the machining amount of the target member can be decreased, so that machining becomes easy, and the influence of machining on other aberrations can be prevented.

In the present invention, it is preferable that the projection optical system is constituted to sequentially have a front group, an aperture stop, and a rear group in this order from the object side. At this time, it is preferable that the target member be arranged in one of the front and rear groups, through which a beam having a smaller numerical aperture passes. With this arrangement, the target member is arranged at a position where the beam has a small spot size for the purpose of imaging. Therefore, the control precision of the residual magnification component and the residual distortion component can be further improved. Furthermore, with this arrangement, the influence of the adjusting method of the present invention on other aberration components can be decreased.

The present invention is preferably arranged such that the target member is located in the front or rear group and farthest from the aperture stop. With this arrangement, the target member is provided at a position where the beam has a small spot size for the

purpose of imaging. Therefore, the control precision of the residual magnification component and the residual distortion component can be further improved. Furthermore, in this arrangement, since the target member is located at the outermost position (closest to the object or the image) of the projection optical system, the arrangement of the lens barrels of the projection optical system can be simplified, thereby facilitating removal and insertion of the target member in the third and fourth steps.

The present invention preferably satisfies an inequality:

$$d/f < 0.07 \quad \dots(1)$$

where d is the distance between an optical member adjacent to a target member and this target member, and f is the focal length of the group in which the target member is located.

This conditional inequality (1) defines the appropriate arrangement of the target member. When this conditional inequality (1) is not satisfied, the operational distance of the projection optical system cannot be sufficiently maintained, which is not preferable. In the conditional inequality (1), it is preferable that the lower limit of d/f be set to 0.001 to satisfy $0.001 < d/f$. If d/f exceeds this lower limit, it may cause interference between a holding

member that holds the target member and a holding member that holds an optical member adjacent to the target member. Then, the degree of freedom in design of the holding members is decreased, which is not preferable.

The present invention preferably satisfies an inequality:

$$-0.005 < \Phi < 0.005 \quad \dots(2)$$

where Φ is the refracting power of the target member. The refracting power Φ of the target member is expressed by $\Phi = 1/f_a$ where f_a is the focal length of the target member.

This conditional inequality (2) defines the range of appropriate refracting powers Φ of the target member so that the target member can be easily mounted. If the target member has a refracting power exceeding the range of the conditional inequality (2), the decentering allowed for the target member becomes strict. Then, the target member must be positioned (the optical axis of the target member must be adjusted) at high precision, which is not preferable. If the refracting power Φ of the target member falls within the range of the conditional inequality (2), the influence of aberrations caused by the mounting error of the target member can be decreased, and the positioning precision of the target member can be set

to almost equal to the machining precision of the holding member of the target member. When these points and easy machinability are considered, the target member is preferably constituted by a plane-parallel plate having no refracting power.

The preferred embodiment of the present invention will be described in detail with reference to the accompanying drawings. Fig. 3 is a diagram schematically showing an arrangement of an exposure apparatus suitably applied to a projection optical apparatus of the present invention. The coordinate system is set as shown in Fig. 3.

Referring to Fig. 3, an illumination optical unit IS uniformly illuminates a reticle R placed on a reticle stage RS with exposure light, e.g., a 365-nm i line, a 248-nm KrF excimer laser, and a 193-nm ArF excimer laser. A distortion correction plate 10 serving as the target member, a holding member 11 for placing the distortion correction plate 10 thereon, and a projection objective lens (projection optical system) PL having a predetermined reduction magnification and substantially telecentric on its two sides are provided below the reticle R. The projection objective lens PL sequentially has a front group G_f of positive refracting power, an aperture stop AS, and a rear group G_R of positive refracting power in this order from the

reticle R side, and the ratio in refracting power of the front group G_F to the rear group G_R corresponds to the reduction magnification of the projection objective lens PL. In this embodiment, the projection objective lens PL is optically designed such that its aberration is corrected including that of the distortion correction plate 10. Accordingly, light from the reticle R illuminated by the illumination optical unit IS reaches a wafer W placed on a wafer stage WS through the distortion correction plate 10 and projection objective lens PL, and forms a reduced image of the reticle R on the wafer W. This wafer stage WS is movable in the X, Y, and Z directions. In this embodiment, the distortion correction plate 10 is constituted by a plane-parallel plate made of a material, e.g., silica glass, that transmits exposure light therethrough.

As shown in, e.g., Fig. 4, the holding member 11 on which the distortion correction plate 10 is placed has an opening for passing exposure light therethrough, and pins 11a to 11c for regulating the distortion correction plate 10 are provided on part of the holding member 11. Accordingly, when the distortion correction plate 10 is abutted against the pins 11a to 11c, the distortion correction plate 10 is positioned.

In this embodiment, of the various aberrations of

the projection objective lens PL, symmetrical components are corrected prior to the random component of the distortion. First, a test reticle TR₁ formed with a predetermined pattern is placed on the reticle stage RS. As shown in, e.g., Fig. 5, the test reticle TR₁ has a pattern area PA₁ provided with a plurality of marks and a light-shielding band LST surrounding the pattern area PA₁. The test reticle TR₁ is subjected to Koehler illumination with the exposure light emerging from the illumination optical unit IS. Light emerging from the illuminated test reticle TR₁ reaches the wafer W coated with a photosensitive material, e.g., a resist, through the distortion correction plate 10 and projection objective lens PL, and forms the pattern image of the test reticle TR₁ on the wafer W. Thereafter, the wafer W is developed, and the resist pattern image obtained by this development is measured by a coordinate measuring machine. The distances between the optical members and the tilt shift of the optical members are adjusted based on the information on the measured resist pattern image, thereby correcting the various aberrations other than the random component of the distortion.

After the various aberrations other than the random component of the distortion are corrected, the random component of the distortion is corrected.

A test reticle TR_2 as shown in Fig. 6 is placed on the reticle stage RS in place of the test reticle TR_1 used for above correction. The test reticle TR_2 has a plurality of cross marks $M_{0,0}$ to $M_{8,8}$ arranged in a matrix form, i.e., arranged on the lattice points of square lattices, within a pattern area PA_2 surrounded by a light-shielding band LST that shields exposure light. The cross marks $M_{0,0}$ to $M_{8,8}$ of the test reticle TR_2 may be formed on the pattern area PA_1 of the test reticle TR_1 . In other words, both the test reticles TR_1 and TR_2 may be employed simultaneously.

As shown in Fig. 3, the test reticle TR_2 on the reticle stage RS is illuminated with the exposure light of the illumination optical unit IS. Light from the test reticle TR_2 reaches the exposure area on the wafer W whose surface is coated with the photosensitive material, e.g., the resist, through the distortion correction plate 10 and projection objective lens PL, and forms the latent images of the plurality of cross marks $M_{0,0}$ to $M_{8,8}$ of the test reticle TR_2 on the wafer W. The exposed wafer W is developed, and the plurality of exposed cross marks $M_{0,0}$ to $M_{8,8}$ are patterned.

Fig. 7 shows the plurality of patterned cross marks in an exposure area EA on the wafer W. In Fig. 7, ideal imaging positions where images are formed when the projection optical system is an ideal optical

system (an optical system having no aberrations) are expressed by intersection points of broken lines. In Fig. 7, a cross mark $P_{0,0}$ corresponds to the image of the cross mark $M_{0,0}$ on the reticle R, a cross mark $P_{1,0}$ corresponds to the image of the cross mark $M_{1,0}$ on the reticle R, and a cross mark $P_{0,1}$ corresponds to the image of the cross mark $M_{0,1}$ on the reticle R. Any other cross mark $M_{i,j}$ and cross mark $P_{i,j}$ correspond to each other in the same manner.

The X- and Y-coordinates of each of the plurality of cross marks $P_{0,0}$ to $P_{8,8}$ formed on the wafer W are measured by the coordinate measuring machine.

In this embodiment, beams emerging from the plurality of cross marks $M_{0,0}$ to $M_{8,8}$ and focused on the plurality of cross marks $P_{0,0}$ to $P_{8,8}$ are shifted to ideal imaging positions by machining the surface of the distortion correction plate 10. The calculation of the surface shape of the practical distortion correction plate 10 will be described.

As shown in Fig. 3, the distortion correction plate 10 of this embodiment is arranged in the optical path between the projection objective lens PL and the reticle R. This position is a position where a beam having a comparatively smaller numerical aperture (N.A.) passes. Thus, in shifting the imaging positions by the distortion correction plate 10, only shifting of

the principal ray of the beam shifted by changing the surface shape of the distortion correction plate 10 need be representatively considered.

A relationship expressed by an equation:

$$w = \beta \cdot L_R \cdot (n - 1) \cdot \theta \quad \dots(3)$$

is established where w is a distortion amount which is a shift amount between the ideal imaging positions and the plurality of cross marks $P_{0,0}$ to $P_{8,8}$ shown in Fig. 7, and θ is the change amount of angle of the normal to the surface of the distortion correction plate 10 at a principal ray passing point where each of the principal rays from the plurality of cross marks $M_{0,0}$ to $M_{8,8}$ passes through the distortion correction plate 10. The angle change amount θ concerns the normal to the surface of the distortion correction plate 10 in a reference state before machining, β is the lateral magnification of the projection optical system, L_R is a distance between the reticle R and the machining target surface of the distortion correction plate 10 along the optical axis, and n is the refractive index of the distortion correction plate 10. In equation (3), the machining target surface of the distortion correction plate 10 is on the wafer W side.

When the distortion correction plate 10 is located in the optical path between the projection objective lens PL and wafer W, a relationship satisfying an

equation:

$$w = L_w \cdot (n-1) \cdot \theta \quad \dots (4)$$

is established where L_w is a distance between the wafer
W and the machining target surface of the distortion
correction plate 10 along the optical axis.

Therefore, the plane normals at principal ray
passing points on the surface of the distortion
correction plate 10 can be obtained from the distortion
amount as a shift amount between the coordinates of the
plurality of cross marks $P_{0,0}$ to $P_{8,8}$ measured by the
coordinate measuring machine described above and the
ideal imaging positions.

Although the plane normals at the respective
principal ray passing points of the distortion
correction plate 10 are determined by the above
procedure, the surface of the distortion correction
plate 10 cannot be obtained as a continuous surface.
Therefore, in this embodiment, a continuous surface
shape is obtained from the plane normals at the
principal ray passing points of the distortion
correction plate 10 that are obtained by the equation
(3) or (4), by using a curved surface interpolation
equation.

Various types of curved surface interpolation
equations are available. In this embodiment, since
plane normals are known and the tangential vectors of

the surface at the principal ray passing points can be calculated from the plane normals, as the curved surface interpolation equation used in this embodiment, the Coons' equation is suitable which extrapolates a curved surface with the coordinate points and tangential vectors of these coordinate points. For example, however, if the tangential vectors θ_0 and θ_1 of adjacent coordinate points Q_0 and Q_1 are equal, as shown in Fig. 8, the extrapolated curved line (curved surface) may wave.

In this embodiment, when the distortion amounts caused by the principal rays that pass through adjacent principal ray passing points are equal, it is effective to equalize the distortion amounts of these adjacent principal ray passing points. If the extrapolated curved line (curved surface) waves, as shown in Fig. 8, the amounts and directions of distortion at adjacent principal ray passing points change over time. Then, not only the random component of the distortion cannot be corrected, but also a random component of this type might be further generated undesirably.

Hence, in this embodiment, in order to equalize the distortion amounts of adjacent principal ray passing points as well, as shown in Fig. 9, the vector component in the Z direction of a tangential vector θ_0 at the coordinate point Q_0 is added, as a height Z_1 in

the Z direction, to the coordinate point Q_1 adjacent to the coordinate point Q_0 . Then, even if the tangential vectors of the adjacent coordinate points Q_0 and Q_1 are equal, the extrapolated curved line becomes almost linear between these coordinate points Q_0 and Q_1 , and the principal rays passing between these coordinate points Q_0 and Q_1 are refracted at almost the same angles. Accordingly, when the distortion amounts of the adjacent principal ray passing points are equal, the distortion amounts can be equalized between these points as well.

The procedure of curved surface complement of this embodiment will be described in detail with reference to Figs. 10 to 14. An X-Y-Z coordinate system is set as shown in Figs. 10 to 14.

[Step 1]

As shown in Fig. 10, an X-Y-Z coordinate system is defined on a target surface 10a of the distortion correction plate 10. In Fig. 10, principal ray passing points $Q_{0,0}$ to $Q_{8,8}$, through which the principal rays of the beams propagating from the plurality of cross marks $M_{0,0}$ to $M_{8,8}$ shown in Fig. 6 toward the plurality of cross marks $P_{0,0}$ to $P_{8,8}$ shown in Fig. 7 pass, are expressed by intersection points of broken lines. The normal vectors at the respective principal ray passing points $Q_{0,0}$ to $Q_{8,8}$ obtained by the above equation (3) are

expressed as $\theta_{i,j}$ (note that in this embodiment $i = 0$ to 8 and $j = 0$ to 8, that is, $\theta_{0,0}$ to $\theta_{8,8}$, and that the X- and Y- components of vector $\theta_{i,j}$ are defined as zero when the direction of the normal vector $\theta_{i,j}$ is equal to the direction of the optical axis), and the heights of the normal vectors in the Z direction at the respective principal ray passing points $Q_{0,0}$ to $Q_{8,8}$ are expressed as $Z_{i,j}$ (note that in this embodiment $i = 0$ to 8 and $j = 0$ to 8, that is, $Z_{0,0}$ to $Z_{8,8}$).

[Step 2]

As shown in Fig. 11, of the principal ray passing points, the principal ray passing point $Q_{0,0}$ at the end point of the Y-axis is defined as the reference in the Z-axis direction, and is set as $Z_{0,0} = 0$.

[Step 3]

The height $Z_{0,1}$ in the Z direction of the tangential vector at the principal ray passing coordinate point $Q_{0,1}$ adjacent to the principal ray passing point $Q_{0,0}$ on the Y-axis is calculated, based on the normal vector $\theta_{0,0}$ of the principal ray passing point $Q_{0,0}$, by the following equation (5):

$$Z_{0,j} = Z_{0,j-1} + \theta_{y_{0,j-1}} \cdot (Y_{0,j} - Y_{0,j-1}) \quad \dots (5)$$

where $\theta_{y_{0,j}}$: the vector component in the Y-axis direction of the normal vector $\theta_{0,j}$ at the principal ray passing point $Q_{0,j}$

$Y_{0,j}$: the component in the Y-axis direction of

the coordinates of the principal ray passing point $Q_{0,j}$ obtained when the principal ray passing point $Q_{0,0}$ is set as the origin

5 In step 3, the height $Z_{0,1}$ in the Z direction of the tangential vector at the principal ray passing point $Q_{0,1}$ is calculated based on the above equation (5) as follows

$$Z_{0,1} = Z_{0,0} + \theta y_{0,0} \cdot (y_{0,1} - y_{0,0})$$

10 [Step 4]

The heights $Z_{0,2}$ to $Z_{0,8}$ in the Z direction of the tangential vectors at the principal ray passing points $Q_{0,2}$ to $Q_{0,8}$ on the Y-axis are calculated based on the above equation (5) in the same manner as in step 3.

15 [Step 5]

The height $Z_{1,0}$ in the Z direction of the tangential vector at the principal ray passing coordinate point $Q_{1,0}$ adjacent to the principal ray passing point $Q_{0,0}$ on the X-axis is calculated, based on the normal vector $\theta_{0,0}$ of the principal ray passing point $Q_{0,0}$, by the following equation (6):

$$20 \quad Z_{i,0} = Z_{i-1,0} + \theta x_{i-1,0} \cdot (x_{i,0} - x_{i-1,0}) \quad \dots (6)$$

where $\theta x_{i,0}$: the vector component in the X-axis direction of the normal vector $\theta_{i,0}$ at the principal ray passing point $Q_{i,0}$

25 $x_{i,0}$: the component in the X-axis direction of

the coordinates of the principal ray
passing point $Q_{1,0}$ obtained when the
principal ray passing point $Q_{0,0}$ is set
as the origin

5 In step 5, the height $Z_{1,0}$ in the Z direction of
the tangential vector at the principal ray passing
point $Q_{1,0}$ is calculated based on the above equation (6)
as follows

$$Z_{1,0} = Z_{0,0} + \theta x_{0,0} \cdot (x_{1,0} - x_{0,0})$$

10 [Step 6]

The heights $Z_{2,0}$ to $Z_{8,0}$ in the Z direction of the
tangential vectors at the principal ray passing points
 $Q_{2,0}$ to $Q_{8,0}$ on the X-axis are calculated based on the
above equation (6) in the same manner as in step 5.

15 [Step 7]

As shown in Fig. 12, the heights $Z_{i,j}$ in the Z
direction of the tangential vectors at the principal
ray passing points $Q_{1,1}$ to $Q_{8,8}$ located between the X- and
Y-axes are sequentially calculated starting with the
one closer to the origin $Q_{0,0}$ based on the following
equation (7):

$$Z_{i,j} = \{ [Z_{i-1,j} + \theta x_{i-1,j} \cdot (x_{i,j} - x_{i-1,j})] + [Z_{i,j-1} + \theta y_{i,j-1} \cdot (y_{i,j} - y_{i,j-1})] \} / 2 \quad \dots (7)$$

20 In step 7, first, the height $Z_{1,1}$ in the Z
25 direction of the tangential vector at the principal ray
passing point $Q_{1,1}$ closest to the origin $Q_{0,0}$ is

calculated. $Z_{1,1}$ is calculated based on the equation (7) as follows

$$Z_{1,1} = \{[Z_{0,1} + \theta x_{0,1} \cdot (x_{1,1} - x_{0,1})] + [Z_{1,0} + \theta y_{1,0} \cdot (y_{1,1} - y_{1,0})]\}/2$$

In step 7, as shown in Fig. 13, after the height $Z_{1,1}$ in the Z direction of the tangential vector at the principal ray passing point $Q_{1,1}$ is calculated, the heights $Z_{1,2}$, $Z_{2,1}$, $Z_{2,2}$, ..., $Z_{1,j}$, ..., and $Z_{8,8}$ in the Z direction of the tangential vectors at the principal ray passing points $Q_{1,2}$, $Q_{2,1}$, $Q_{2,2}$, ..., $Q_{1,j}$, ..., and $Q_{8,8}$ are sequentially calculated starting with the one closer to the origin $Q_{0,0}$ based on the above equation (7).

[Step 8]

Based on the heights $Z_{0,0}$ to $Z_{8,8}$ at the principal ray passing points $Q_{0,0}$ to $Q_{8,8}$ obtained through steps 1 to 7, the X- and Y-coordinates of the principal ray passing points $Q_{0,0}$ to $Q_{8,8}$, and the tangential vectors at the principal ray passing points $Q_{0,0}$ to $Q_{8,8}$ obtained from the plane normal vectors $\theta_{0,0}$ to $\theta_{8,8}$ at the principal ray passing points $Q_{0,0}$ to $Q_{8,8}$, a curved surface is formed in accordance with the Coons' patching method. More specifically, the control points of the Coons' patching method are determined as the X-, Y-, and Z-coordinates of the principal ray passing points $Q_{0,0}$ to $Q_{8,8}$, and the tangential vectors of the

control points are determined as the tangential vectors calculated from the plane normal vectors $\theta_{0,0}$ to $\theta_{8,8}$ at the principal ray passing points $Q_{0,0}$ to $Q_{8,8}$.

A curved surface as shown in, e.g., Fig. 14, can be obtained by curved surface interpolation in accordance with the Coons' patching method of step 8.

In above steps 1 to 8, the height $Z_{0,0}$ in the Z direction of the tangential vector at the point $Q_{0,0}$ located at the edge of the target surface 10a is set as 0 (step 2), the heights $Z_{0,1}$ to $Z_{0,8}$ and $Z_{1,0}$ to $Z_{8,0}$ in the Z direction of the tangential vectors at the points $Q_{0,1}$ to $Q_{0,8}$ and the points $Q_{1,0}$ to $Q_{8,0}$ on the Y- and X-axes, respectively, present at the edges of the target surface 10a are calculated (steps 3 to 6), and thereafter the heights $Z_{i,j}$ ($i \neq 0, j \neq 0$) in the Z direction of the tangential vectors at points other than the points on the Y- and Z-axes are calculated (Steps 7 and 8). Thus, farther from the point $Q_{0,0}$, the larger the error in the calculated value, and the sizes of the errors of the calculated values are not symmetric with respect to the central point $Q_{4,4}$ of the target surface 10a through which the optical axis of the projection objective lens PL passes.

For this reason, the heights $Z_{i,j}$ may be calculated in the accordance with the following procedure. First, in step 2, the height $Z_{4,4}$ in the Z direction of the

tangential vector at the point $Q_{4,4}$ located at the center of the target surface 10a is defined as 0. In steps 3 to 6, the heights $Z_{4,0}$ to $Z_{4,3}$, $Z_{4,5}$ to $Z_{4,8}$, and $Z_{0,4}$ to $Z_{3,4}$, $Z_{5,4}$ to $Z_{8,4}$ in the Z direction of the tangential vectors at the points $Q_{4,0}$ to $Q_{4,3}$, $Q_{4,5}$ to $Q_{4,8}$, $Q_{0,4}$ to $Q_{3,4}$, and $Q_{5,4}$ to $Q_{8,4}$ on axes extending through the central point $Q_{4,4}$ and parallel to the Y- or Z-axis are calculated. Thereafter, in steps 7 and 8, the heights $Z_{i,j}$ ($i \neq 4$, $j \neq 4$) in the Z direction of the tangential vectors at points other than the points on the axes extending through the point $Q_{4,4}$ and parallel to the Y- or X-axis are calculated.

When the distortion measurement points, i.e., the marks on the test reticles, are not arranged on the lattice points of the square lattices, the heights in the Z direction and the plane normal vectors at lattice points on square lattices located between the respective measurement points are interpolated. More specifically, the height in the Z direction and the plane normal vector at a lattice point can be obtained by summing the heights in the Z direction and the plane normal vectors at a plurality of measurement points surrounding these lattice points while weighting them with the distances between the measurement points and the lattice points.

In above steps 1 to 8, only information inside the

distortion measurement points is used. However, in order to further smooth the surface of the distortion correction plate 10 serving as the target member, the lattice points may be set on the outer side (a side remote from the optical axis) of the principal ray passing points corresponding to the distortion measurement points, and the heights in the Z direction and the plane normal vectors at these lattice points may be extrapolated from the height in the Z direction and the plane normal vector at the outermost principal ray passing point.

The distortion correction plate 10 is removed from the projection optical apparatus shown in Fig. 3, and the surface of the removed distortion correction plate 10 is machined based on surface shape data of the distortion correction plate 10 which is calculated through steps 1 to 8. The distortion correction plate 10 of this embodiment has a random surface that waves irregularly, in order to correct the random component of the distortion. Accordingly, in this embodiment, a polishing machine as shown in Fig. 15 is used. A coordinate system as indicated in Fig. 15 is employed.

Referring to Fig. 15, the distortion correction plate 10 is placed on a stage 21 movable in the X and Y directions, and the end portion of the distortion correction plate 10 is abutted against a pin 21a on the

stage 21. A driver 22 for moving the stage 21 in the X and Y directions is controlled by a controller 20. A detector 30 comprising an encoder, an interferometer, and the like is provided to the stage 21 to detect the position of the stage 21 in the X and Y directions when the stage 21 is moved. A detection signal output from the detector 30 is transmitted to the controller 20.

A polisher 23 is attached to one end of a rotating shaft 25 through a holding portion 24 and is rotatable about the Z direction in Fig. 15 as the rotation axis. A motor 26 controlled by the controller 20 is mounted to the other end of the rotating shaft 25. A bearing 27 that rotatably supports the rotating shaft 25 is provided to a support portion 28 fixed to a main body (not shown) to be movable in the Z direction. A motor 29 controlled by the controller 20 is mounted to the support portion 28. When the motor 29 is operated, the bearing 27 is moved in the Z direction, and accordingly the polisher 23 is moved in the Z direction. The holding portion 24 for holding the polisher 23 is provided with a sensor (not shown) which detects a contact pressure between the abrasion tray 23 and the distortion correction plate 10. An output from this sensor is transmitted to the controller 20.

The operation of the polishing machine shown in Fig. 15 will be briefly described. Surface shape data

obtained through steps 1 to 8 is input to the controller 20. Thereafter, the controller 20 moves the stage 21 in the X and Y directions through the driver 22 while it rotates the polisher 23. More specifically, the polisher 23 is moved on the target surface 10a of the distortion correction plate 10 in the X and Y directions. At this time, the amount of abrasion of the target surface 10a of the distortion correction plate 10 is determined by the contact pressure between the target surface 10a and the polisher 23 and the residence time of the polisher 23.

An anti-reflection film is coated, by vapor deposition, on the distortion correction plate 10 machined by the abrading machine shown in Fig. 15, and the machined distortion correction plate 10 is placed on the holding member 11 of the projection optical apparatus shown in Fig. 3. In the polishing machine of Fig. 15, the polisher 23 is fixed in the X and Y directions. However, the polisher 23 may be moved in the X and Y directions in place of moving the stage 21 in the X and Y directions. Alternatively, a small tool (see Fig. 16) may be used in place of the polisher 23.

With this embodiment described above, correction of the random component of distortion, which has conventionally been impossible only with adjustment of the respective optical members constituting the

projection optical system, can be performed easily.

In the above embodiment, as the plane-parallel plate having no refracting power is used as the distortion correction plate 10, the decentering precision of the distortion correction plate can be moderated. Then, even if positioning is performed by the holding member 11 as shown in Fig. 4, i.e., even if positioning is determined by the machining precision of the holding member 11, sufficiently high optical performance can be achieved. As the distortion correction plate 10 is a plane-parallel plate, it can be machined easily. When a lens having a predetermined curvature is used as the distortion correction plate 10, this lens preferably has a low refracting power due to the reason described above.

In the above embodiment, as the distortion correction plate 10 is arranged on the reticle R side (enlargement side) where the beam has a smaller numerical aperture, only shift of the principal ray is considered. However, when the distortion correction plate 10 is arranged on the wafer W side (reduction side), the machining amount of the distortion correction plate 10 is preferably determined by considering the influence of the size of the beam on the distortion correction plate 10. Also, in order to further improve the precision of distortion correction,

even if the distortion correction plate 10 is arranged on the reticle R side, the machining amount is preferably determined by considering the influence of the size of the beam size on the distortion correction plate 10.

In the above embodiment, the distortion correction plate 10 is mounted in the optical path for measurement to decrease the adverse influence caused by the parts precision of the distortion correction plate 10.

However, for measurement, a dummy component different from the distortion correction plate as the target member may be mounted in the optical path. In this case, however, the parts precision of the dummy component must be high.

In the above embodiment, since the distortion correction plate 10 is an optical member which is placed closest to the reticle of all the optical members constituting the projection objective lens PL, the operation of mounting and removing the distortion correction plate 10 in and from the optical path of the projection objective lens PL can be performed easily.

In the above embodiment, the distortion correction plate 10 is positioned with precision which is determined by the machining precision of the holding member 11. In order to perform higher-precision correction, a predetermined mark may be provided to

part of the distortion correction plate 10, so that the location of the distortion correction plate 10 with respect to the holding member 11 (with respect to the projection objective system PL) is optically detected.

5 At this time, the mark is desirably provided to the distortion correction plate 10 at a position through which exposure light does not pass.

Fig. 16 briefly shows the adjusting method of the present invention that has been described so far. In Fig. 16, the distortion correction plate 10 is mounted in the optical path of the projection objective system PL, and the distortion is measured. Subsequently, the shape of the distortion correction plate 10 is calculated based on this measured distortion by using software that calculates an aspherical shape.

15 Thereafter, the distortion correction plate 10 is machined by using a small tool or the like so that it has the calculated shape. When the distortion correction plate 10 machined in this manner is mounted in the optical path of the projection objective system PL again, the distortion on the surface of the wafer W is almost 0.

20 Fig. 17 briefly shows how to calculate the shape of the distortion correction plate 10 from distortion data. In Fig. 17, the amounts with which the plane normals at the respective points on the distortion

correction plate 10 must be controlled are calculated based on the distortion data obtained by measurement. Subsequently, the shape of a curved surface that the machining target should have is calculated such that it satisfies the control amounts calculated in this manner.

From the invention thus described, it will be obvious that the invention may be varied in many ways. Such variations are not to be regarded as a departure from the spirit and scope of the invention, and all such modifications as would be obvious to one skilled in the art are intended for inclusion within the scope of the following claims.

The basic Japanese Application No. 009687/1995 (7-009687) filed on January 25, 1995 is hereby incorporated by reference.